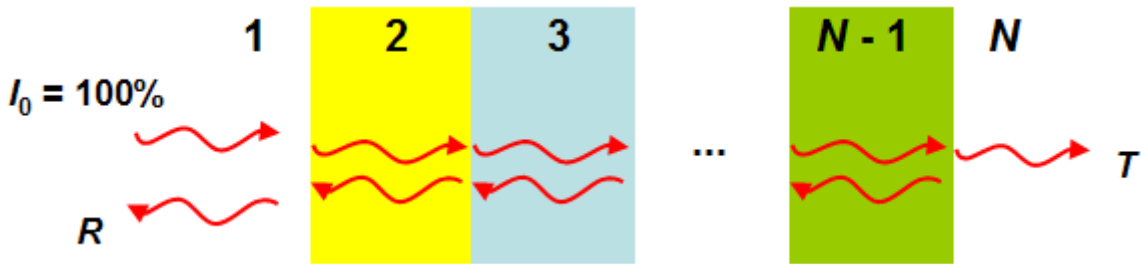


## Transfer Matrix Method

Light propagation in a multilayered film structure (**Figure 1**) can be calculated based on transfer matrix method.



**Figure 1.** A multilayered structure.

Assume all the materials are non-magnetic ( $\mu_r = 1$ )

First define the propagation direction, which is illustrated in **Figure 2**. When wave propagates along the  $x$  axis from left to right, the expression of the electric field is

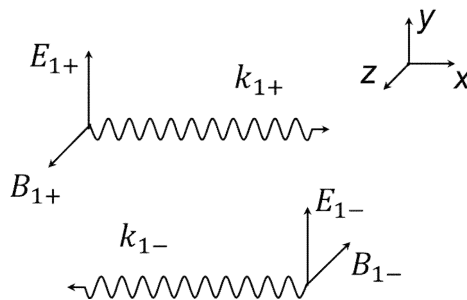
$$E_{1+} = |E_{1+}| \exp(ik_1x) \quad (S1)$$

when wave propagates in the opposite direction, it becomes

$$E_{1-} = |E_{1-}| \exp(-ik_1x) \quad (S2)$$

and

$$k_1 = \frac{2\pi}{\lambda} n_1 \quad (S3)$$



**Figure 2.** Defining the positive direction of propagation.

Thin-film filters consist of boundaries between different homogenous media, as shown in

**Figure 3.** At the interface of media 1 and 2, the boundary conditions are

$$\begin{cases} E_1^{\parallel} = E_2^{\parallel} \\ B_1^{\parallel} = B_2^{\parallel} \end{cases} \quad (\text{S4})$$

and  $B = \frac{n}{c} E$

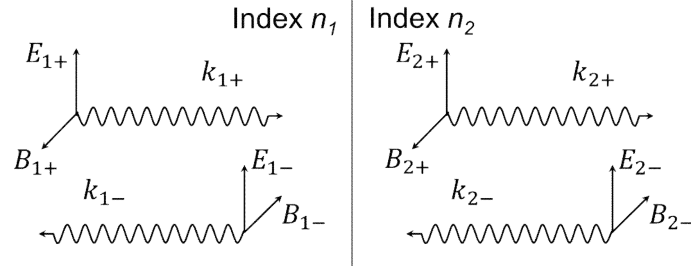
Therefore

$$\begin{cases} E_{1+} + E_{1-} = E_{2+} + E_{2-} \\ B_{1+} - B_{1-} = B_{2+} - B_{2-} \end{cases} \rightarrow \begin{cases} E_{1+} + E_{1-} = E_{2+} + E_{2-} \\ n_1(E_{1+} - E_{1-}) = n_2(E_{2+} - E_{2-}) \end{cases} \quad (\text{S5})$$

which can be written in matrix form:

$$\begin{bmatrix} E_{1+} \\ E_{1-} \end{bmatrix} = \begin{bmatrix} \frac{1}{2} \left( 1 + \frac{n_2}{n_1} \right) & \frac{1}{2} \left( 1 - \frac{n_2}{n_1} \right) \\ \frac{1}{2} \left( 1 - \frac{n_2}{n_1} \right) & \frac{1}{2} \left( 1 + \frac{n_2}{n_1} \right) \end{bmatrix} \begin{bmatrix} E_{2+} \\ E_{2-} \end{bmatrix} = D_{12} \begin{bmatrix} E_{2+} \\ E_{2-} \end{bmatrix} \quad (\text{S6})$$

$D_{12}$  is a matrix to describe the process at the 1-2 interface.



**Figure 3.** Plane wave incident on a single interface.

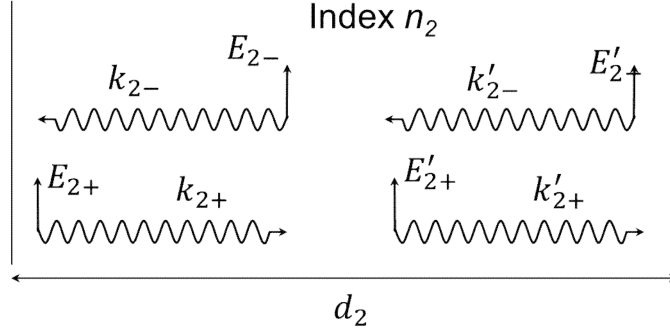
Light propagation in homogenous medium 2 (thickness  $d_2$ ) has the relations (**Figure 4**)

$$\begin{cases} E'_{2+} = |E_{2+}| \exp(ik_2 x + ik_2 d_2) = E_{2+} \exp(i \frac{2\pi}{\lambda} n_2 d_2) \\ E'_{2-} = |E_{2-}| \exp(-ik_2 x - ik_2 d_2) = E_{2-} \exp(-i \frac{2\pi}{\lambda} n_2 d_2) \end{cases} \quad (\text{S7})$$

so

$$\begin{bmatrix} E_{2+} \\ E_{2-} \end{bmatrix} = \begin{bmatrix} \exp(-i\frac{2\pi}{\lambda}n_2d_2) & 0 \\ 0 & \exp(i\frac{2\pi}{\lambda}n_2d_2) \end{bmatrix} \begin{bmatrix} E'_{2+} \\ E'_{2-} \end{bmatrix} = P_2 \begin{bmatrix} E'_{2+} \\ E'_{2-} \end{bmatrix} \quad (\text{S8})$$

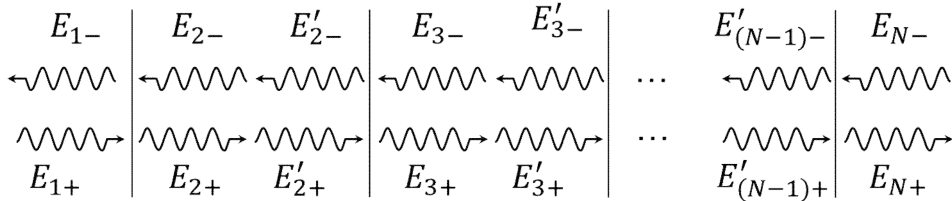
$P_{12}$  is a matrix to describe the propagation in the medium 2.



**Figure 4.** Plane wave propagating in a homogeneous medium.

**Figure 5** shows model geometry of light traveling through  $N$  layers. The following matrix relation can be deduced referring to Equation S6 and S8:

$$\begin{aligned} \begin{bmatrix} E_{1+} \\ E_{1-} \end{bmatrix} &= D_{12} \begin{bmatrix} E_{2+} \\ E_{2-} \end{bmatrix} = D_{12} P_2 \begin{bmatrix} E'_{2+} \\ E'_{2-} \end{bmatrix} = D_{12} P_2 D_{23} \begin{bmatrix} E_{3+} \\ E_{3-} \end{bmatrix} \\ &= \dots = D_{12} P_2 D_{23} P_3 \dots P_{N-1} D_{(N-1)N} \begin{bmatrix} E_{N+} \\ E_{N-} \end{bmatrix} \\ &= \begin{bmatrix} M_{11} & M_{12} \\ M_{21} & M_{22} \end{bmatrix} \begin{bmatrix} E_{N+} \\ E_{N-} \end{bmatrix} \end{aligned} \quad (\text{S9})$$



**Figure 5.** Plane wave traveling through a number of layers.

and there is no back reflected light at the last medium  $N$ , so

$$E_{N-} = 0 \rightarrow \begin{cases} E_{1+} = M_{11}E_{N+} \\ E_{1-} = M_{21}E_{N+} \end{cases} \quad (\text{S10})$$

The irradiance intensity is related to the Poynting vector

$$I = \frac{1}{2} \text{Re}(\mathbf{E} \times \mathbf{H}^*) \quad (\text{S11})$$

or

$$I \propto n |E|^2 \quad (\text{S12})$$

Reflectance  $R$  is defined as the ratio of the reflected and incident irradiances and transmittance  $T$  as the ratio of the transmitted and incident irradiances:

$$R = \left| \frac{E_{1-}}{E_{1+}} \right|^2 = \left| \frac{M_{21}}{M_{11}} \right|^2 \quad (\text{S13})$$

$$T = \frac{n_N}{n_1} \left| \frac{E_{N+}}{E_{1+}} \right|^2 = \frac{n_N}{n_1} \left| \frac{1}{M_{11}} \right|^2 \quad (\text{S14})$$

For absorptive materials, use the complex  $\tilde{n}$  to replace  $n$

$$\tilde{n} = n + i\kappa, \text{ if we define wave function } E \sim \exp(ikx) \quad (\text{S15})$$

*note:* use  $\tilde{n} = n - i\kappa$ , if we define wave function  $E \sim \exp(-ikx)$

$\kappa$  - extinction coefficient

For oblique angles (**Figures 6 and 7**), boundary conditions are

$$\begin{cases} n_1^2 E_1^\perp = n_2^2 E_2^\perp \\ E_1^\parallel = E_2^\parallel \\ B_1^\perp = B_2^\perp \\ B_1^\parallel = B_2^\parallel \end{cases} \quad (\text{S16})$$

and from Snell's law,

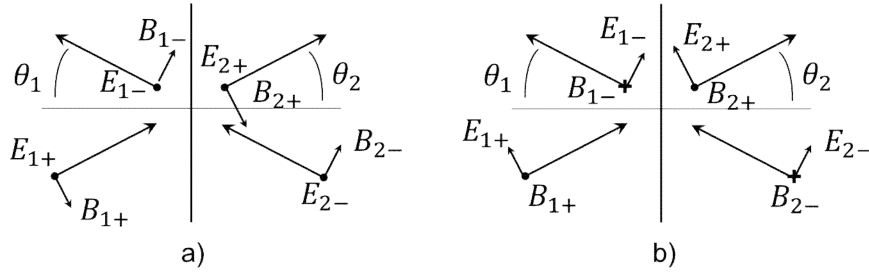
$$n_1 \sin \theta_1 = n_2 \sin \theta_2 \quad (\text{S17})$$

For s-polarised light, in the notation of **Figure 6**, is

$$\begin{aligned} \begin{bmatrix} 1 & 1 \\ n_1 \cos \theta_1 & -n_1 \cos \theta_1 \end{bmatrix} \begin{bmatrix} E_{1+} \\ E_{1-} \end{bmatrix} &= \begin{bmatrix} 1 & 1 \\ n_2 \cos \theta_2 & -n_2 \cos \theta_2 \end{bmatrix} \begin{bmatrix} E_{2+} \\ E_{2-} \end{bmatrix} \\ D_{12} &= \begin{bmatrix} 1 & 1 \\ n_1 \cos \theta_1 & -n_1 \cos \theta_1 \end{bmatrix}^{-1} \begin{bmatrix} 1 & 1 \\ n_2 \cos \theta_2 & -n_2 \cos \theta_2 \end{bmatrix} \end{aligned} \quad (\text{S18})$$

and p-polarised light can be described as

$$\begin{aligned} \begin{bmatrix} \cos \theta_1 & \cos \theta_1 \\ n_1 & -n_1 \end{bmatrix} \begin{bmatrix} E_{1+} \\ E_{1-} \end{bmatrix} &= \begin{bmatrix} \cos \theta_2 & \cos \theta_2 \\ n_2 & -n_2 \end{bmatrix} \begin{bmatrix} E_{2+} \\ E_{2-} \end{bmatrix} \\ D_{12} &= \begin{bmatrix} \cos \theta_1 & \cos \theta_1 \\ n_1 & -n_1 \end{bmatrix}^{-1} \begin{bmatrix} \cos \theta_2 & \cos \theta_2 \\ n_2 & -n_2 \end{bmatrix} \end{aligned} \quad (\text{S19})$$



**Figure 6.** a) Convention defining the positive directions of electric and magnetic vectors for s-polarised light (TE waves). b) Convention defining the positive directions of electric and magnetic vectors for p-polarised light (TM waves).

Light of oblique incidence propagating in homogeneous medium (**Figure 7**) are analogous to that of normal incidence:

$$\begin{bmatrix} E_{2+} \\ E_{2-} \end{bmatrix} = \begin{bmatrix} \exp(-i \frac{2\pi}{\lambda} n_2 d_2 \cos \theta_2) & 0 \\ 0 & \exp(i \frac{2\pi}{\lambda} n_2 d_2 \cos \theta_2) \end{bmatrix} \begin{bmatrix} E'_{2+} \\ E'_{2-} \end{bmatrix} = P_2 \begin{bmatrix} E'_{2+} \\ E'_{2-} \end{bmatrix}. \quad (\text{S20})$$

**Figure 7.** a) s-polarised light and b) p-polarised light propagating in homogeneous medium with oblique angles.